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Overall Values of Conventional Discrepancy Indices in the Presence of Random Positional Errors: Crystal with Similar Atoms

BY S. PARTHASARATHY AND M. N. PONNUSWAMY

Department of Crystallography and Biophysics, University of Madras, Guindy Campus, Madras 600 025, India*

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Abstract

The overall values of the conventional discrepancy indices based on structure amplitudes [*i.e.* $R(F)$] and intensities [*i.e.* $R(I)$] are evaluated as functions of the mean positional error $\langle |\Delta r| \rangle$ and the fractional contribution of the known atoms to the local mean intensity (*i.e.* σ_1^2) for crystals containing a large number of similar atoms. The results are tabulated for both the centrosymmetric and non-centrosymmetric cases.

1. Introduction

The use of discrepancy indices in the various stages of crystal structure analysis is well known. Of the various indices that have been proposed (Srinivasan & Parthasarathy, 1976; hereafter SP, 1976), the conventional discrepancy indices [denoted by $R(F)$ and $R(I)$] are the ones normally computed in crystallographic programs. Wilson (1950) worked out the maximum probable values of $R(F)$ for centrosymmetric and non-centrosymmetric (hereafter *C* and *NC*) cases when the trial structure is of the unrelated *complete* (*i.e.* $\sigma_1^2 = 1$)† type. He also considered the effect of a single badly misplaced atom on $R(F)$ and $R(I)$ when the trial structure is of the complete type (Wilson, 1969).

Luzzati (1952) considered the effect of random positional errors on $R(F)$ and obtained $R(F)$ as a function of $\sin \theta$ for different fixed values of the mean positional error $\langle |\Delta r| \rangle$. His results, however, apply only for a complete model (*i.e.* $\sigma_1^2 = 1$). Srinivasan, Raghupathy Sarma & Ramachandran (1963) worked out the values of $R(F)$ for two limiting situations, namely, the related (*i.e.* $\langle |\Delta r| \rangle = 0$) and the unrelated (*i.e.* $\langle |\Delta r| \rangle$ very large) cases and their results apply to a complete as well as an incomplete type of trial structure (*i.e.* $0 < \sigma_1^2 \leq 1$). Thus the *overall values* of $R(F)$ and $R(I)$ [denoted by $\bar{R}(F)$ and $\bar{R}(I)$, respectively] applicable for the general case of an *imperfectly related* (*i.e.* $\langle |\Delta r| \rangle$ finite) *incomplete* (*i.e.* $0 < \sigma_1^2 \leq 1$) type are not available. These overall values are important because: (1) crystallographers judge the correctness of trial structures generally from the overall values of the conventional *R* indices computed with all the observed independent reflections as a single group; (2) the trial structures met with in practice are such that they often account for only part of the structure (*i.e.* $\sigma_1^2 < 1$) and, further, they involve atoms with random positional errors. In the presence of random positional errors the *R* indices are expected to be monotonically increasing functions of $(\sin \theta)/\lambda$ (hereafter *S*). In this paper we shall therefore obtain the theoretical overall values of $R(F)$ and $R(I)$ as functions of σ_1^2 and $\langle |\Delta r| \rangle$ for the general case of an imperfectly related incomplete model. The results obtained here are applicable only for crystals containing similar atoms.

* Contribution No. 485.

† See § 2 for a definition of σ_1^2 .

2. Theoretical considerations

Consider a crystal (C or NC) consisting of N atoms in the unit cell of which P are known. Let $\langle |\Delta \mathbf{r}| \rangle$ be the mean positional error of the P atoms of the trial structure. Let $|F_N|$ and $|F_P^c|$ be the structure factor magnitudes of a reflection \mathbf{H} for the crystal and trial structures respectively. Let $I_N (= |F_N|^2)$ and $I_P^c (= |F_P^c|^2)$ be the corresponding intensities. σ_1^2 , denoting the fractional contribution to the local mean intensity from the P atoms of the trial structure, is defined by

$$\sigma_1^2 = \sigma_P^2 / \sigma_N^2, \quad (1)$$

where

$$\sigma_\alpha^2 = \sum_{k=1}^{\alpha} f_{\alpha k}^2, \quad \alpha = N \text{ or } P. \quad (2)$$

Since for a structure with equal atoms $\sigma_\alpha^2 = \alpha f^2$ ($\alpha = N$ or P), we can write

$$\sigma_1^2 = P/N, \quad (3)$$

which is independent of S . The normalized structure amplitudes y_N and y_P^c and the corresponding intensities z_N and z_P^c are defined by

$$\begin{aligned} z_N &= y_N^2 = |F_N|^2 / \sigma_N^2, \\ z_P^c &= [y_P^c]^2 = |F_P^c|^2 / \sigma_P^2. \end{aligned} \quad (4)$$

We shall presently derive the theoretical expression required for the evaluation of $\bar{R}(F)$. Since the corresponding expression for $\bar{R}(I)$ can be derived by a similar method we shall give only the final result for this case.

The overall value of the conventional discrepancy index based on structure amplitudes is defined by

$$\bar{R}(F) = \frac{\sum |F_N| - |F_P^c|}{\sum |F_N|}, \quad (5)$$

where the summations are over all the independent observed reflections. If the reflections are divided into groups based on the values of S , we can rewrite (5) as

$$\bar{R}(F) = \frac{\sum_j \sum_i ||F_N| - |F_P^c||_{ij}}{\sum_j \sum_i |F_N|_{ij}}, \quad (6)$$

where the summation over i is carried out over reflections in a given range of S and that over j is carried out over the various ranges of S . Making use of the variables y_N and y_P^c [see (4)], we can rewrite (6) as

$$\bar{R}(F) = \frac{\sum_j \sigma_{Nj} \sum_i |y_N - \sigma_1 y_P^c|_{ij}}{\sum_j \sigma_{Nj} \sum_i y_{Nij}}, \quad (7)$$

where σ_{Nj} denotes the value of σ_N in the j th range of S .

In writing (7) we have taken the value of σ_N for all reflections in a given range of S to be constant and this would be practically true when the range of S is sufficiently small. If n_j denotes the number of reflections in the j th range of S , we can rewrite (7) as

$$\bar{R}(F) = \frac{\sum_j \sigma_{Nj} n_j \langle |y_N - \sigma_1 y_P^c| \rangle_j}{\sum_j \sigma_{Nj} n_j \langle y_N \rangle_j}. \quad (8)$$

For a crystal with similar atoms $\langle y_N \rangle$ can be obtained from the Wilson (1949) distributions as

$$\begin{aligned} \langle y_N \rangle &= (2/\pi)^{1/2} \quad \text{for } C, \\ &= (\pi/2)^{1/2} \quad \text{for } NC, \end{aligned} \quad (9)$$

and thus $\langle y_N \rangle$ is independent of S . For equal atom structures we can take σ_N^2 to be Nf^2 . We can therefore rewrite (8) as

$$\bar{R}(F) = \frac{\sum_j f_j n_j R_j(y)}{\sum_j f_j n_j}, \quad (10)$$

where $R_j(y)$ is the value of $R(y)$ in the j th interval of S and $R(y)$ is defined by

$$R(y) = \frac{\langle |y_N - \sigma_1 y_P^c| \rangle}{\langle y_N \rangle}. \quad (11)$$

If we make the partitioning of the whole range of S into infinitesimally small intervals, then the summation can be replaced by an integration. The number of reflections in the range between S and $S + dS$ will be proportional to the volume $4\pi H^2 dH$ of reciprocal space between shells of radii H and $H + dH$ where $H = 2S$. This volume is evidently $32\pi S^2 dS$. If the data consist of reflections in the range $0 < S \leq S_{\max}$ we can rewrite (10) as

$$\bar{R}(F) = \frac{\int_0^{S_{\max}} f(S) S^2 R(y) dS}{\int_0^{S_{\max}} f(S) S^2 dS}. \quad (12)$$

From the results of Srinivasan & Ramachandran (1965), $R(y)$ defined in (11) can be interpreted as an R index for a point atom structure taking into account the incompleteness of the trial structure. From (11) it is clear that $R(y)$ can be evaluated from a knowledge of the joint *probability density function* (hereafter pdf) of y_N and y_P^c as

$$R(y) = \frac{1}{\beta} \int_0^\infty \int_0^\infty |y_N - \sigma_1 y_P^c| P(y_N, y_P^c) dy_N dy_P^c, \quad (13)$$

where β is the value of $\langle y_N \rangle$ as given in (9). The function $P(y_N, y_P^c)$ for the C case is known to be (SP, 1976)

$$P(y_N, y_P^c) = \frac{2}{\pi\sigma_B} \exp\left[-\frac{1}{2\sigma_B^2}(y_N^2 + y_P^c{}^2)\right] \times \cosh\left[\frac{\sigma_A y_N y_P^c}{\sigma_B^2}\right], \quad (14)$$

where

$$\sigma_A = \sigma_1 D, \quad \sigma_B = (1 - \sigma_A^2)^{1/2}, \quad (15)$$

and

$$D = \exp(-\pi^3 S^2 \langle |\Delta r| \rangle^2). \quad (16)$$

The function $P(y_N, y_P^c)$ for the NC case is (SP, 1976)

$$P(y_N, y_P^c) = \frac{4y_N y_P^c}{\sigma_B^2} \exp\left[-\frac{(y_N^2 + y_P^c{}^2)}{\sigma_B^2}\right] I_0\left[\frac{2\sigma_A y_N y_P^c}{\sigma_B^2}\right], \quad (17)$$

where I_0 is the modified Bessel function of the first kind of order zero. Substituting (14) [or (17) for the NC

case] in (13) and carrying out the resulting integrations we can obtain the value of $R(y)$. However, it is not possible to evaluate the integrals in (13) in a closed form. Numerical evaluation of (13) can be facilitated by changing the variables to

$$u = y_N/(1 + y_N), \quad v = y_P^c/(1 + y_P^c). \quad (18)$$

We can then rewrite (13) as

$$R(y) = \frac{1}{\beta} \int_0^1 \int_0^1 \left| \frac{1-u}{1-u} - \sigma_1 \frac{v}{1-v} \right| P\left[\frac{u}{1-u}, \frac{v}{1-v}\right] \times \frac{du dv}{(1-u)^2 (1-v)^2}, \quad (19)$$

where we have to use (14) or (17) according as the crystal is C or NC , respectively. From (19) and (14) it is clear that $R(y)$ depends on σ_1 and D . For a given trial structure, σ_1^2 is a fixed quantity. Hence, for a fixed value of σ_1^2 the integrals in (19) can be evaluated numerically for different fixed values of D , say $D = 0, 0.01, 0.02, \dots, 1.0$. From the values of $R(y)$ thus obtained, the overall value $\bar{R}(F)$ for a given trial structure (*i.e.* $\langle |\Delta r| \rangle$ fixed) can be worked out as explained below.

Table 1. Value of $\bar{R}(F)$ as a function of σ_1^2 and $\langle |\Delta r| \rangle$: centrosymmetric case

$\langle \Delta r \rangle$	0.20	0.30	0.40	0.50	0.55	0.60	0.65	0.70	0.75	0.80	0.85	0.90	0.95	1.00
0.00	71.2	66.7	62.6	58.1	55.7	53.1	50.3	47.1	43.7	39.8	35.0	30.2	25.8	0.0
0.01	71.2	66.8	62.7	58.2	55.8	53.2	50.4	47.2	43.8	39.9	35.1	30.3	25.9	1.1
0.02	71.2	66.8	62.7	58.2	55.8	53.2	50.4	47.2	43.8	39.9	35.1	30.3	25.9	1.2
0.03	71.3	66.8	62.7	58.3	55.9	53.3	50.5	47.3	43.9	40.0	35.2	30.4	26.0	1.3
0.04	71.3	66.9	62.8	58.3	56.0	53.4	50.6	47.4	44.0	40.1	35.3	30.5	26.1	1.4
0.05	71.3	66.9	62.8	58.3	56.0	53.4	50.6	47.4	44.0	40.1	35.3	30.5	26.1	1.5
0.06	71.4	67.1	63.0	58.4	56.1	53.5	50.7	47.5	44.1	40.2	35.4	30.6	26.2	1.6
0.07	71.4	67.1	63.0	58.4	56.1	53.5	50.7	47.5	44.1	40.2	35.4	30.6	26.2	1.7
0.08	71.4	67.1	63.0	58.4	56.1	53.5	50.7	47.5	44.1	40.2	35.4	30.6	26.2	1.8
0.09	71.4	67.1	63.0	58.4	56.1	53.5	50.7	47.5	44.1	40.2	35.4	30.6	26.2	1.9
0.10	71.4	67.1	63.0	58.4	56.1	53.5	50.7	47.5	44.1	40.2	35.4	30.6	26.2	2.0
0.11	71.7	67.8	63.6	58.9	56.7	54.1	51.3	48.1	44.7	40.8	36.0	31.2	26.7	2.1
0.12	71.8	68.0	63.7	59.0	56.8	54.2	51.4	48.2	44.8	40.9	36.1	31.3	26.8	2.2
0.13	71.9	68.2	63.9	59.1	57.0	54.3	51.5	48.3	44.9	41.0	36.2	31.4	26.9	2.3
0.14	72.0	68.3	64.0	59.2	57.1	54.4	51.6	48.4	45.0	41.1	36.3	31.5	27.0	2.4
0.15	72.1	68.5	64.2	59.3	57.2	54.5	51.7	48.5	45.1	41.2	36.4	31.6	27.1	2.5
0.16	72.2	68.6	64.3	59.4	57.3	54.6	51.8	48.6	45.2	41.3	36.5	31.7	27.2	2.6
0.17	72.2	68.6	64.3	59.4	57.3	54.6	51.8	48.6	45.2	41.3	36.5	31.7	27.2	2.7
0.18	72.3	68.7	64.4	59.5	57.4	54.7	51.9	48.7	45.3	41.4	36.6	31.8	27.3	2.8
0.19	72.4	68.8	64.5	59.6	57.5	54.8	52.0	48.8	45.4	41.5	36.7	31.9	27.4	2.9
0.20	72.4	68.8	64.5	59.6	57.5	54.8	52.0	48.8	45.4	41.5	36.7	31.9	27.4	3.0
0.21	72.5	68.9	64.6	59.7	57.6	54.9	52.1	48.9	45.5	41.6	36.8	32.0	27.5	3.1
0.22	72.5	68.9	64.6	59.7	57.6	54.9	52.1	48.9	45.5	41.6	36.8	32.0	27.5	3.2
0.23	72.6	69.0	64.7	59.8	57.7	55.0	52.2	49.0	45.6	41.7	36.9	32.1	27.6	3.3
0.24	72.6	69.0	64.7	59.8	57.7	55.0	52.2	49.0	45.6	41.7	36.9	32.1	27.6	3.4
0.25	72.7	69.1	64.8	59.9	57.8	55.1	52.3	49.1	45.7	41.8	37.0	32.2	27.7	3.5
0.26	72.7	69.1	64.8	59.9	57.8	55.1	52.3	49.1	45.7	41.8	37.0	32.2	27.7	3.6
0.27	72.8	69.2	64.9	60.0	57.9	55.2	52.4	49.2	45.8	41.9	37.1	32.3	27.8	3.7
0.28	72.8	69.2	64.9	60.0	57.9	55.2	52.4	49.2	45.8	41.9	37.1	32.3	27.8	3.8
0.29	72.9	69.3	65.0	60.1	58.0	55.3	52.5	49.3	45.9	42.0	37.2	32.4	27.9	3.9
0.30	72.9	69.3	65.0	60.1	58.0	55.3	52.5	49.3	45.9	42.0	37.2	32.4	27.9	4.0
0.31	73.0	69.4	65.1	60.2	58.1	55.4	52.6	49.4	46.0	42.1	37.3	32.5	28.0	4.1
0.32	73.0	69.4	65.1	60.2	58.1	55.4	52.6	49.4	46.0	42.1	37.3	32.5	28.0	4.2
0.33	73.1	69.5	65.2	60.3	58.2	55.5	52.7	49.5	46.1	42.2	37.4	32.6	28.1	4.3
0.34	73.1	69.5	65.2	60.3	58.2	55.5	52.7	49.5	46.1	42.2	37.4	32.6	28.1	4.4
0.35	73.1	69.5	65.2	60.3	58.2	55.5	52.7	49.5	46.1	42.2	37.4	32.6	28.1	4.5
0.36	73.2	69.6	65.3	60.4	58.3	55.6	52.8	49.6	46.2	42.3	37.5	32.7	28.2	4.6
0.37	73.2	69.6	65.3	60.4	58.3	55.6	52.8	49.6	46.2	42.3	37.5	32.7	28.2	4.7
0.38	73.3	69.7	65.4	60.5	58.4	55.7	52.9	49.7	46.3	42.4	37.6	32.8	28.3	4.8
0.39	73.3	69.7	65.4	60.5	58.4	55.7	52.9	49.7	46.3	42.4	37.6	32.8	28.3	4.9
0.40	73.4	69.8	65.5	60.6	58.5	55.8	53.0	49.8	46.4	42.5	37.7	32.9	28.4	5.0
0.41	73.4	69.8	65.5	60.6	58.5	55.8	53.0	49.8	46.4	42.5	37.7	32.9	28.4	5.1
0.42	73.5	69.9	65.6	60.7	58.6	55.9	53.1	49.9	46.5	42.6	37.8	33.0	28.5	5.2
0.43	73.5	69.9	65.6	60.7	58.6	55.9	53.1	49.9	46.5	42.6	37.8	33.0	28.5	5.3
0.44	73.6	70.0	65.7	60.8	58.7	56.0	53.2	50.0	46.6	42.7	37.9	33.1	28.6	5.4
0.45	73.6	70.0	65.7	60.8	58.7	56.0	53.2	50.0	46.6	42.7	37.9	33.1	28.6	5.5
0.46	73.7	70.1	65.8	60.9	58.8	56.1	53.3	50.1	46.7	42.8	38.0	33.2	28.7	5.6
0.47	73.7	70.1	65.8	60.9	58.8	56.1	53.3	50.1	46.7	42.8	38.0	33.2	28.7	5.7
0.48	73.8	70.2	65.9	61.0	58.9	56.2	53.4	50.2	46.8	42.9	38.1	33.3	28.8	5.8
0.49	73.8	70.2	65.9	61.0	58.9	56.2	53.4	50.2	46.8	42.9	38.1	33.3	28.8	5.9
0.50	73.9	70.3	66.0	61.1	59.0	56.3	53.5	50.3	46.9	43.0	38.2	33.4	28.9	6.0
0.51	73.9	70.3	66.0	61.1	59.0	56.3	53.5	50.3	46.9	43.0	38.2	33.4	28.9	6.1
0.52	74.0	70.4	66.1	61.2	59.1	56.4	53.6	50.4	47.0	43.1	38.3	33.5	29.0	6.2
0.53	74.0	70.4	66.1	61.2	59.1	56.4	53.6	50.4	47.0	43.1	38.3	33.5	29.0	6.3
0.54	74.1	70.5	66.2	61.3	59.2	56.5	53.7	50.5	47.1	43.2	38.4	33.6	29.1	6.4
0.55	74.1	70.5	66.2	61.3	59.2	56.5	53.7	50.5	47.1	43.2	38.4	33.6	29.1	6.5
0.56	74.2	70.6	66.3	61.4	59.3	56.6	53.8	50.6	47.2	43.3	38.5	33.7	29.2	6.6
0.57	74.2	70.6	66.3	61.4	59.3	56.6	53.8	50.6	47.2	43.3	38.5	33.7	29.2	6.7
0.58	74.3	70.7	66.4	61.5	59.4	56.7	53.9	50.7	47.3	43.4	38.6	33.8	29.3	6.8
0.59	74.3	70.7	66.4	61.5	59.4	56.7	53.9	50.7	47.3	43.4	38.6	33.8	29.3	6.9
0.60	74.4	70.8	66.5	61.6	59.5	56.8	54.0	50.8	47.4	43.5	38.7	33.9	29.4	7.0
0.61	74.4	70.8	66.5	61.6	59.5	56.8	54.0	50.8	47.4	43.5	38.7	33.9	29.4	7.1
0.62	74.5	70.9	66.6	61.7	59.6	56.9	54.1	50.9	47.5	43.6	38.8	34.0	29.5	7.2
0.63	74.5	70.9	66.6	61.7	59.6	56.9	54.1	50.9	47.5	43.6	38.8	34.0	29.5	7.3
0.64	74.6	71.0	66.7	61.8	59.7	57.0	54.2	51.0	47.6	43.7	38.9	34.1	29.6	7.4
0.65	74.6	71.0	66.7	61.8	59.7	57.0	54.2	51.0	47.6	43.7	38.9	34.1	29.6	7.5
0.66	74.7	71.1	66.8	61.9	59.8	57.1	54.3	51.1	47.7	43.8	39.0	34.2	29.7	7.6
0.67	74.7	71.1	66.8	61.9	59.8	57.1	54.3	51.1	47.7	43.8	39.0	34.2	29.7	7.7
0.68	74.8	71.2	66.9	62.0	59.9	57.2	54.4	51.2	47.8	43.9	39.1	34.3	29.8	7.8
0.69	74.8	71.2	66.9	62.0	59.9	57.2	54.4	51.2	47.8	43.9	39.1	34.3	29.8	7.9
0.70	74.9	71.3	67.0	62.1	60.0	57.3	54.5	51.3	47.9	44.0	39.2	34.4	29.9	8.0
0.71	74.9	71.3	67.0	62.1	60.0	57.3	54.5	51.3	47.9	44.0	39.2	34.4	29.9	8.1
0.72	75.0	71.4	67.1	62.2	60.1	57.4	54.6	51.4	48.0	44.1	39.3	34.5	30.0	8.2
0.73	75.0	71.4	67.1	62.2	60.1	57.4	54.6	51.4	48.0	44.1	39.3	34.5	30.0	8.3
0.74	75.1	71.5	67.2	62.3	60.2	57.5	54.7	51.5	48.1	44.2	39.4	34.6	30.1	8.4
0.75	75.1	71.5	67.2	62.3	60.2	57.5	54.7	51.5	48.1	44.2	39.4	34.6	30.1	8.5
0.76	75.2	71.6	67.3	62.4	60.3	57.6	54.8	51.						

Since a given trial structure of a crystal is characterized by fixed values of σ_1 and $\langle |\Delta \mathbf{r}| \rangle$, for the evaluation of $\bar{R}(F)$ from (12), σ_1 and $\langle |\Delta \mathbf{r}| \rangle$ are to be treated as fixed quantities. The integral on the right-hand side of (12) is to be evaluated numerically. For this the values of $R(y)$ are needed at discrete values of S . This can in turn be obtained by first calculating the relevant values of D from (16) and then by interpolation.

The overall value of the conventional R index based on intensities is defined by

$$\bar{R}(I) = \frac{\sum |I_N - I_P|}{\sum I_N} \quad (20)$$

By following a procedure similar to that employed for $R(F)$ and using the known result that $\langle y_N^2 \rangle = 1$ it can be shown that

$$\bar{R}(I) = \frac{\int_0^{S_{\max}} f^2(S) S^2 R(z) dS}{\int_0^{S_{\max}} f^2(S) S^2 dS} \quad (21)$$

where

$$R(z) = \langle |y_N^2 - \sigma_1^2 y_P^2| \rangle = \int_0^1 \int_0^1 \left| \left(\frac{u}{1-u} \right)^2 - \sigma_1^2 \left(\frac{v}{1-v} \right)^2 \right| \times P \left(\frac{u}{1-u}, \frac{v}{1-v} \right) \frac{du dv}{(1-u)^2 (1-v)^2} \quad (22)$$

The procedure for the evaluation of $\bar{R}(I)$ for any given trial structure is similar to that discussed earlier for $\bar{R}(F)$.

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Thermal Diffuse Scattering for Molecular Crystals: Errors in X-ray Diffraction Intensities and Atomic Parameters

BY P. A. KROON AND AAFJE VOS

Laboratorium voor Chemische Fysica, Rijksuniversiteit Groningen, Nijenborgh 16, 9747 AG Groningen, The Netherlands

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Abstract

First-order TDS calculations have been made for naphthalene at 100 K to judge the suitability of different models for calculating TDS corrections used

3. Discussion of the theoretical results

The overall values of $R(F)$ and $R(I)$ as functions of σ_1^2 and $\langle |\Delta \mathbf{r}| \rangle$ (in Å) were evaluated by the procedure discussed in § 2 by taking f in (12) and (21) to be the scattering factor of the C atom. S_{\max} in (12) and (21) is taken to be 0.6485 which is the maximum value of $(\sin \theta)/\lambda$ corresponding to Cu $K\alpha$ radiation. The results thus obtained for $\bar{R}(F)$ and $\bar{R}(I)$ are given in Tables 1 and 2 respectively for the centrosymmetric case, and in Tables 3 and 4 for the non-centrosymmetric case. Since a major portion of an organic or a biomolecule is composed of C atoms and since the scattering powers of O and N are comparable with C, these results could be expected to hold good for organic crystal structures. A study of these tables shows that $\bar{R}(I)$ would be preferable to $\bar{R}(F)$ particularly in the conventional refinement stage.

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